

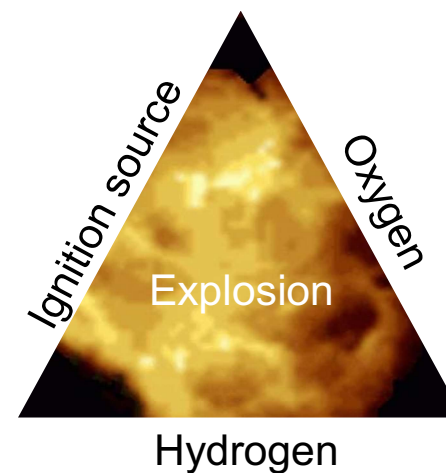
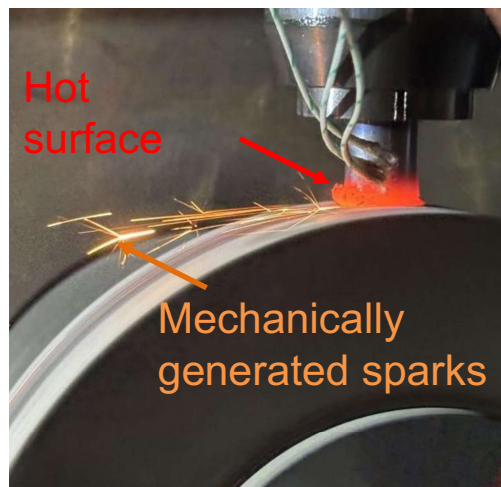
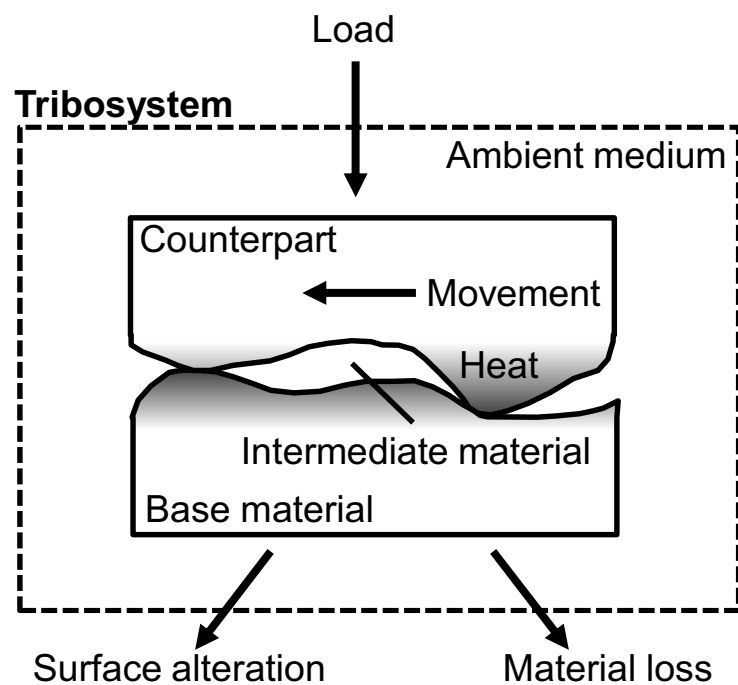
# Ignition of hydrogen due to friction

Florian Baumann, Carola Schierding, Michael Hau,  
Maurice Neumann, Michael Beyer

FABIG TECHNICAL MEETING  
24 & 25 March 2026, London, UK

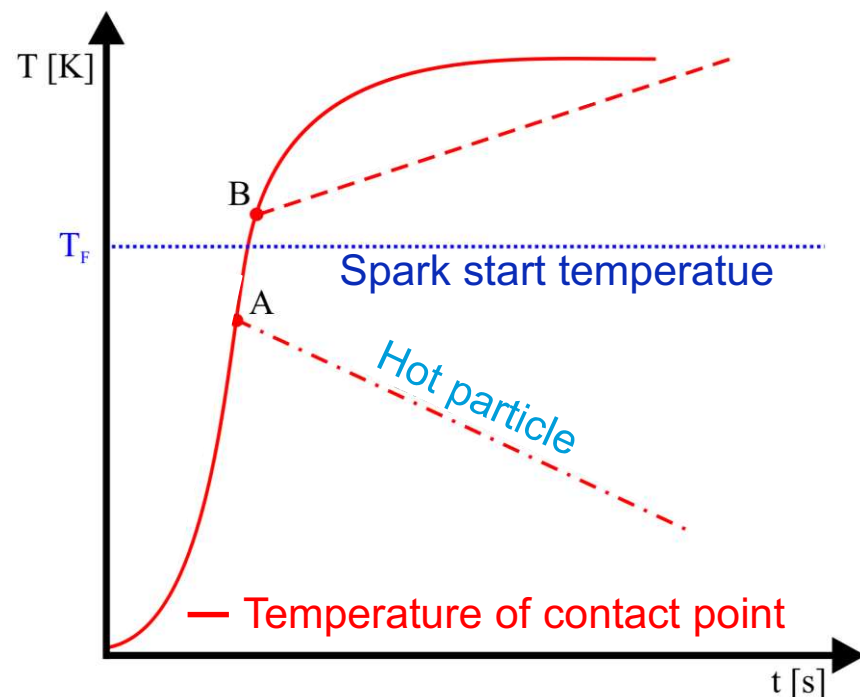


# Introduction



# Mechanically generated sparks

Difference between „Hot particles“ and „Mechanically generated sparks“



Hot particle:

Temperature of contact point  $< T_F$

→ no exothermic reaction

→ cools down during flight

→ no ignition known due to hot particles

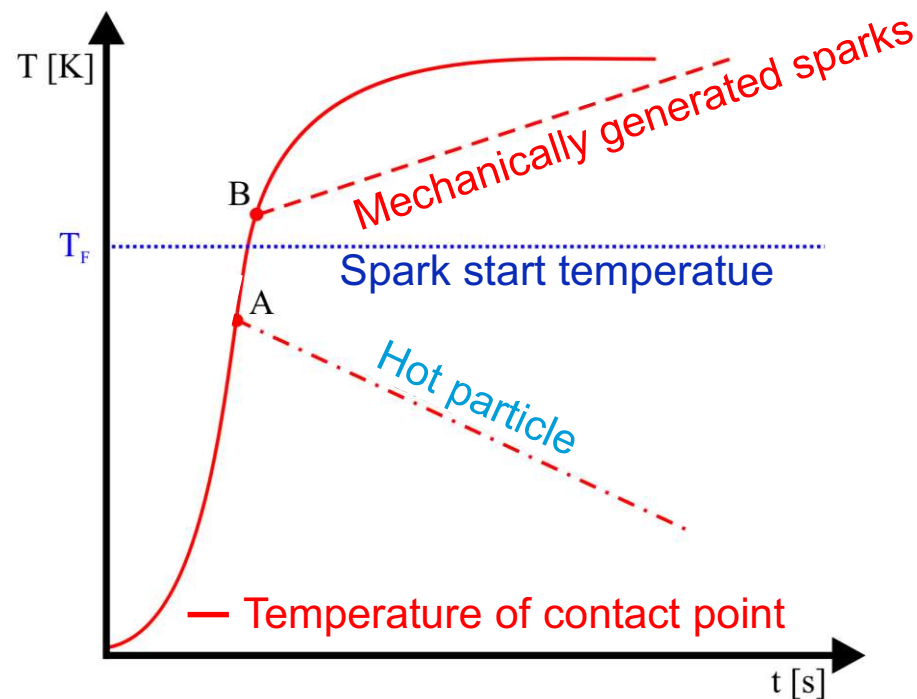
Below  $T_F$ :

Ignitions are only possible due to hot surfaces

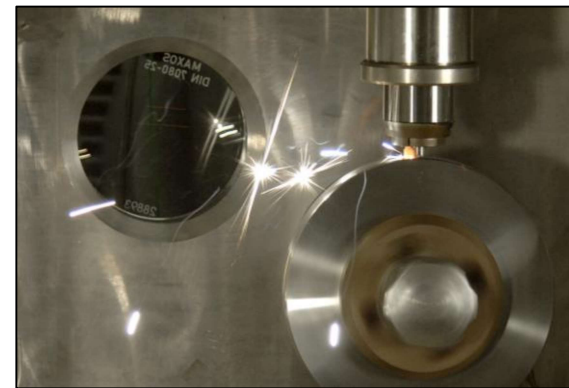
Reference: MEYER, L. Die Entstehung von heißen Oberflächen in metallischen Reibsituationen und ihre Zündwirksamkeit: PTB-Bericht PTB-Ex-9, Dissertation. Magdeburg, 2018

# Mechanically generated sparks

Difference between „Hot particles“ and „Mechanically generated sparks“

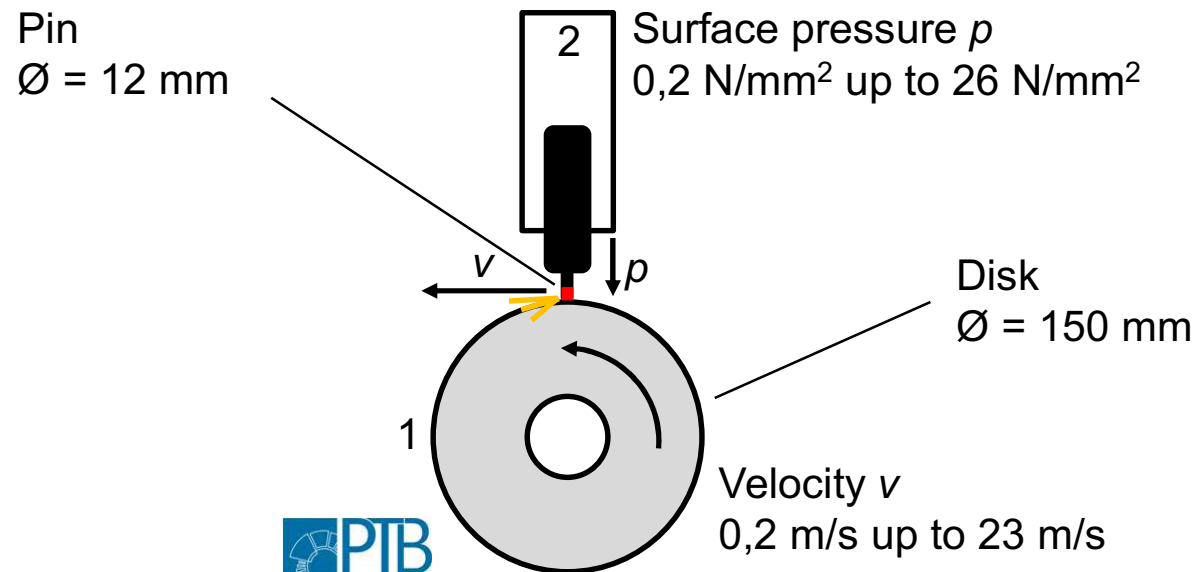


Mechanically generated sparks :  
Temperature of contact point  $> T_F$   
→ Sufficient energy for an exothermic reaction  
→ Rise in temperature up to over 900 °C  
→ Ignition



Reference : MEYER, L. Die Entstehung von heißen Oberflächen in metallischen Reibsituationen und ihre Zündwirksamkeit: PTB-Bericht PTB-Ex-9, Dissertation. Magdeburg, 2018

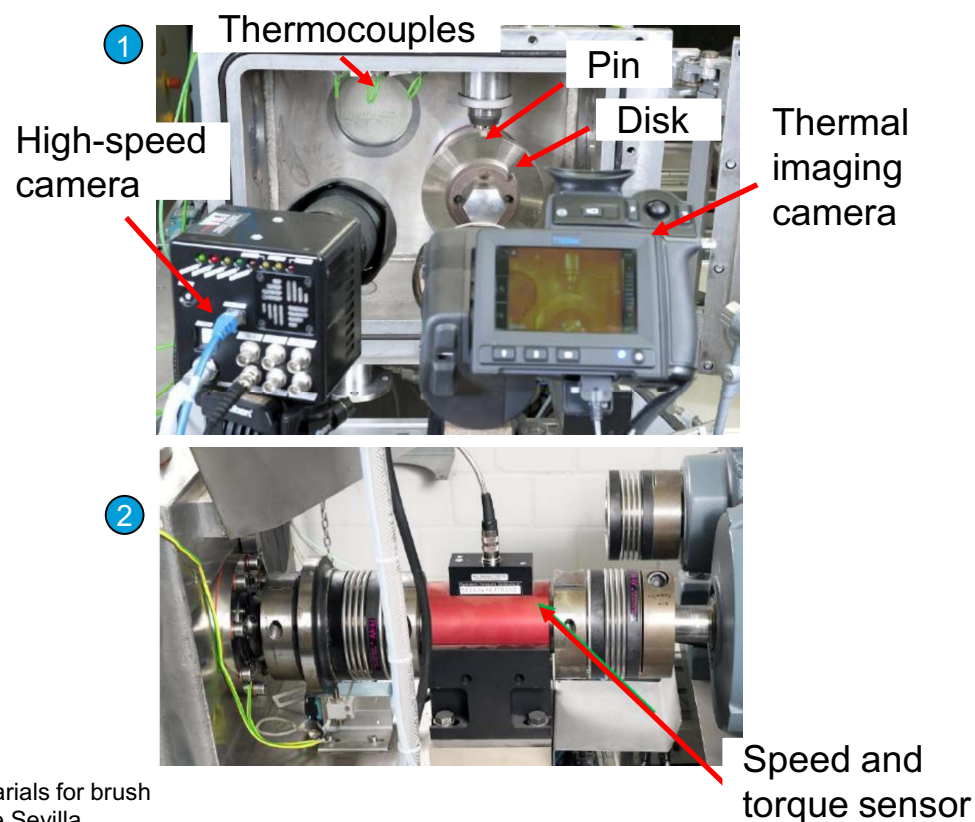
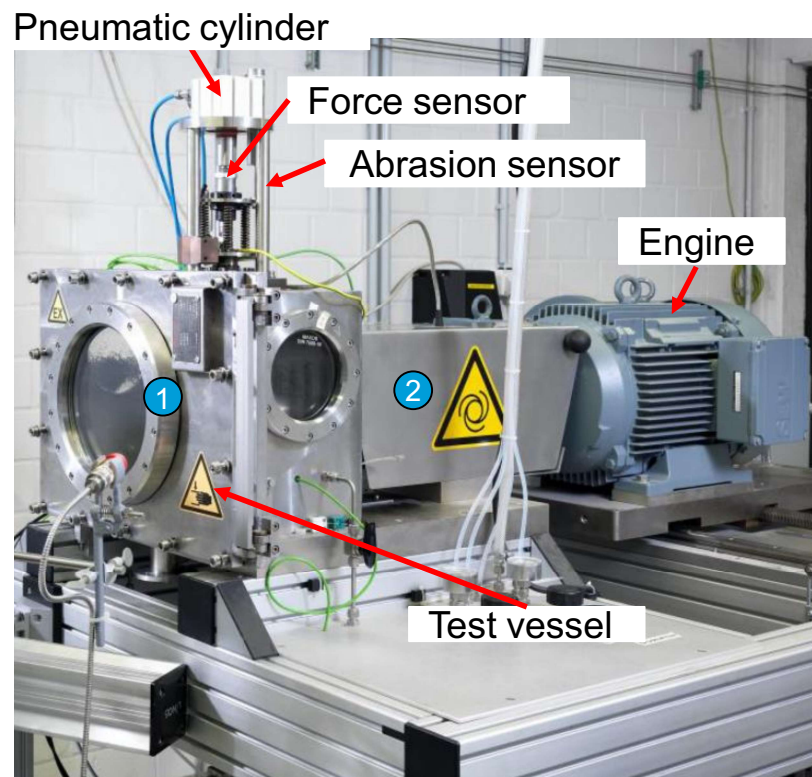
# Set up for experiments



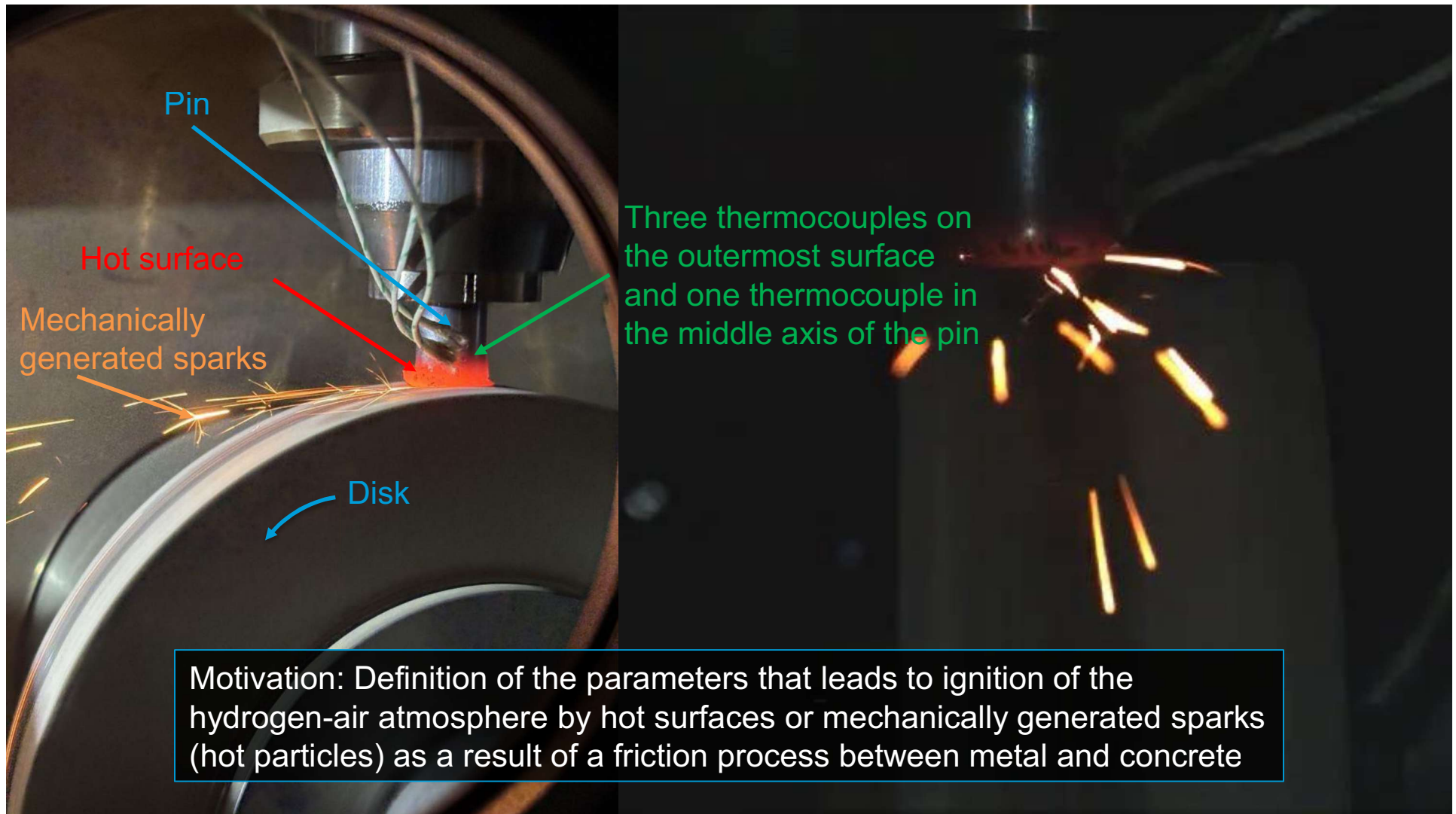
- 1: Rotating disk mounted on a shaft
- 2: Cylinder for applying contact pressure



# Set up for experiments



Reference: Aguilera Cabezas, F. J. (2022): Non-spark and conventional materials for brush cutters: mechanical and thermal behavior. Master-Thesis PTB/Universidad Se Sevilla



# Material combinations



 - Concrete

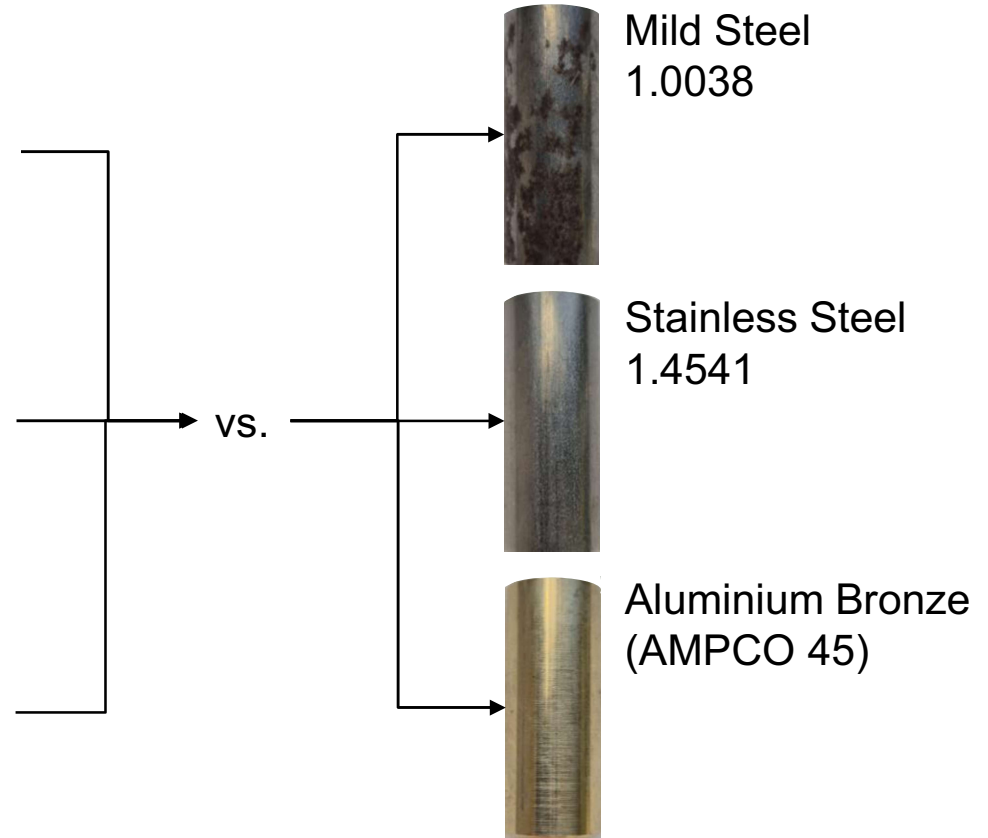
Cut from paving slabs using  
a water jet cutter



 BAM - Concrete  
Additive 81% (Okrilla quartz  
sand, various grain sizes)  
12% Cement  
6,8 % Water  
0,2 % Flow agent



 BAM - Concrete  
With 5% Corundum





# Challenges - Concrete

## Aim:

Constant start conditions

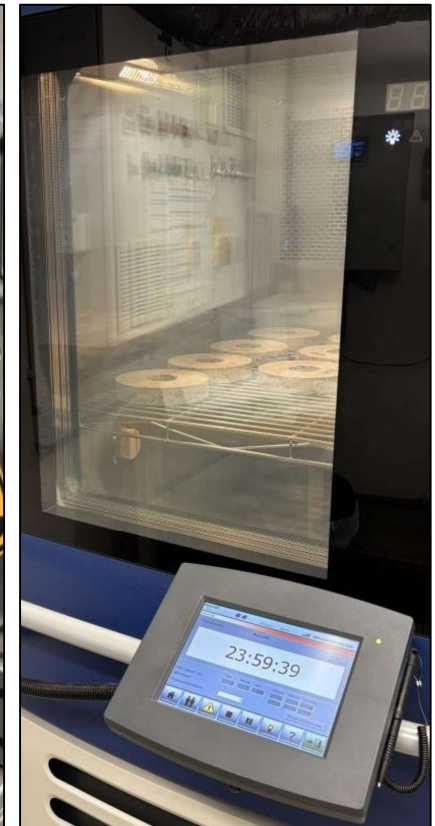
## Problems:

- High humidity and condensation in the test vessel due to the release of pore water from the concrete disks  
(experiment without hydrogen)

## Solutions:

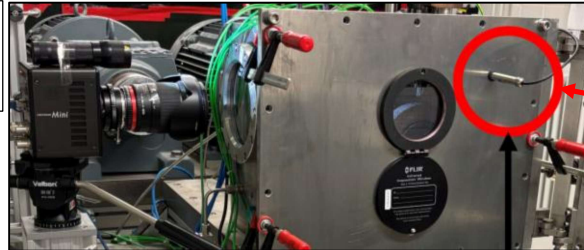
- Drying the concrete disks (24 h at 120 °C)  
→ Weight loss up to 24 g

Note: Another drying cycle will not result in any further weight loss



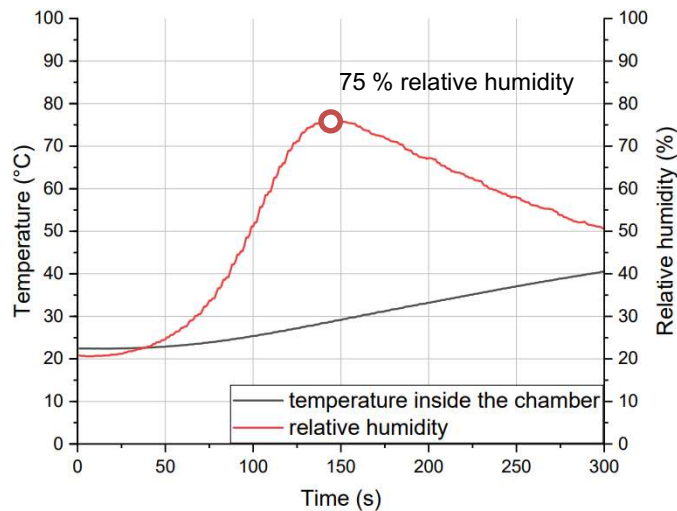
# Challenges - Concrete

Experiment with mild steel (1.0038),  
 $v = 5 \text{ m/s}$ ,  $p = 2 \text{ N/mm}^2$

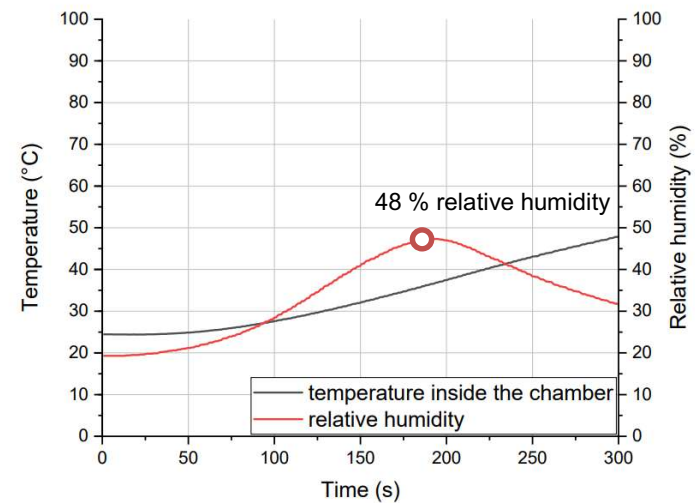


Sensor for  
humidity and temperature

Not dried PTB-Concrete-Disk

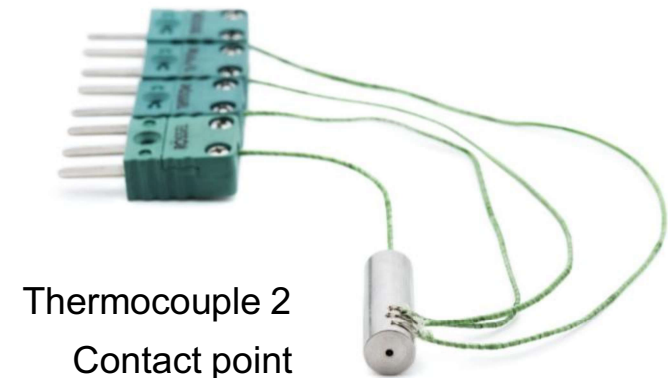
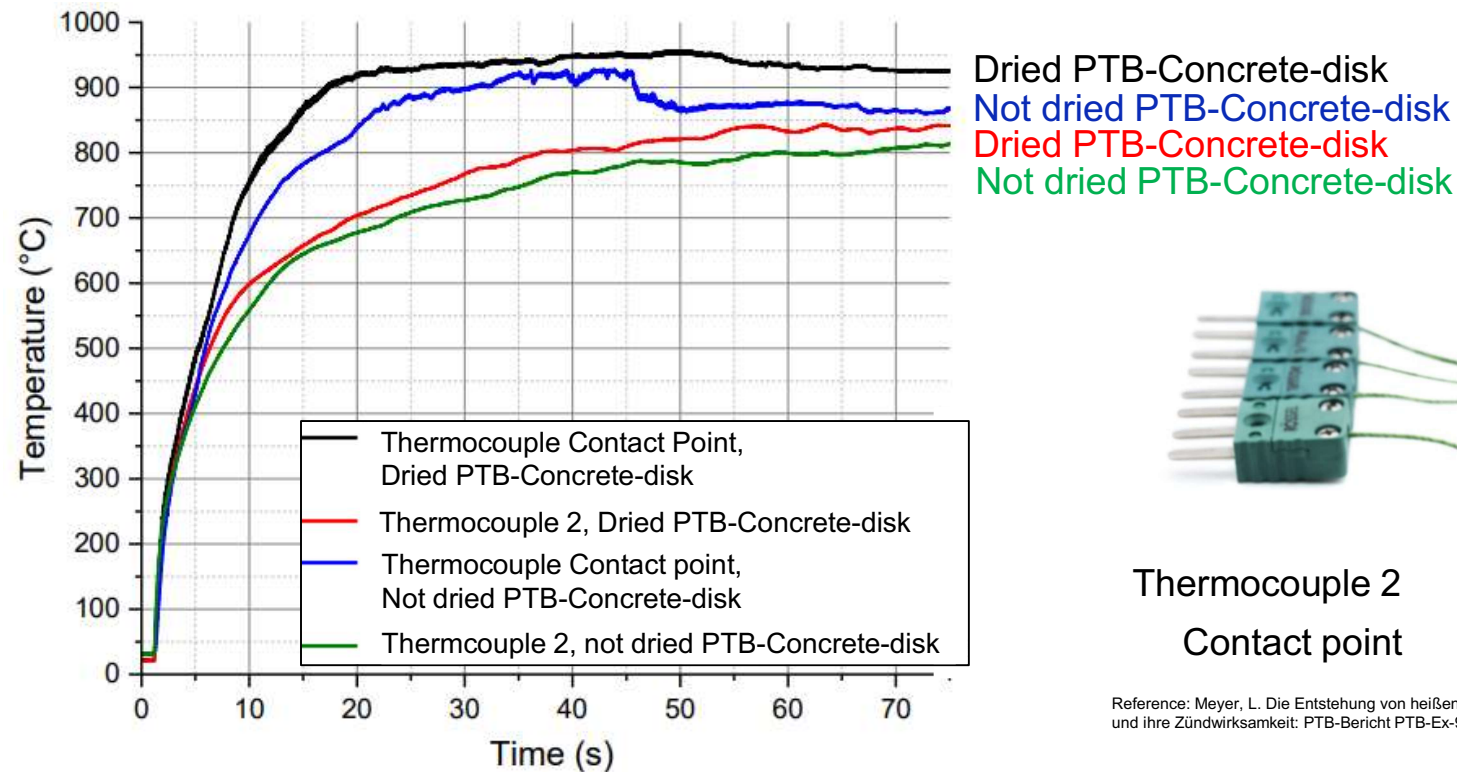


dried PTB-Concrete-Disk



# Challenges - Concrete

Experiment with PTB-Concrete (disk) and mild steel 1.0038 (pin),  $v = 5 \text{ m/s}$ ,  $p = 5 \text{ N/mm}^2$



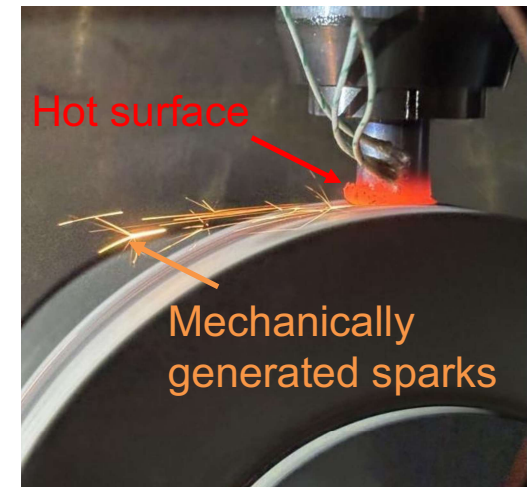
Reference: Meyer, L. Die Entstehung von heißen Oberflächen in metallischen Reibsituationen und ihre Zündwirksamkeit: PTB-Bericht PTB-Ex-9, Dissertation. Magdeburg, 2018.

# Hydrogen concentration

**Why 10 Vol.-% of hydrogen in air, and not the stoichiometric mixture of 29.5Vol.-%?**

**Hot surface:** Hydrogen has high heat conductivity (0.184 W/m·K at 20 °C) and can be used as a cooling medium  
→ Concentrations below 29.5% Vol.-% result in earlier ignition

**Mechanically generated sparks:** The oxidation of the hot particles reduces the oxygen concentration and changes the mixture locally towards stoichiometric conditions



## Verified by:

- Previous experiments using this test setup with 10 Vol.-%, 20 Vol.-% and 30 Vol.-% of hydrogen in air

Reference : - TITMAN, H.: The ignition of explosive gas mixtures by friction, 1954

- Welzel, F.: Die Entstehung von Zündquellen durch Reibvorgänge und deren Zündwirksamkeit in explosionsfähigen Gas/Luft-Atmosphären. 2014

- Meyer, L. Die Entstehung von heißen Oberflächen in metallischen Reibsituationen und ihre Zündwirksamkeit: PTB-Bericht PTB-Ex-9, Dissertation. Magdeburg, 2018

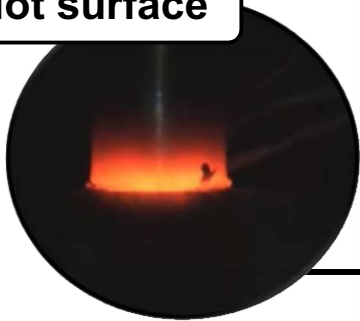
- Experiments on small hot surfaces

Reference : - Mevel, R.; Melguizo-Gavilanes, J.; Boeck, L. R.; Shepherd, J. E.: Experimental and numerical study of the ignition of hydrogen-air mixtures by a localized stationary hot surface. In: International Journal of Heat and Fluid Flow 76 (2019), pp. 154-169

# Ignition source

The ignition source depends on the material:

## Hot surface



### PIN:

- Stainless Steel 1.4541
- Aluminium Bronze
- AMPCO45

vs.

### DISK:

- PTB Concrete,
- BAM Concrete
- BAM Concrete with 5 % Corundum

## Mechanically generated sparks



### PIN:

- Mild Steel 1.0038

vs.

### DISK:

- PTB Concrete,
- BAM Concrete
- BAM Concrete with 5 % Corundum

The corundum has  
no influence on the  
ignition source!



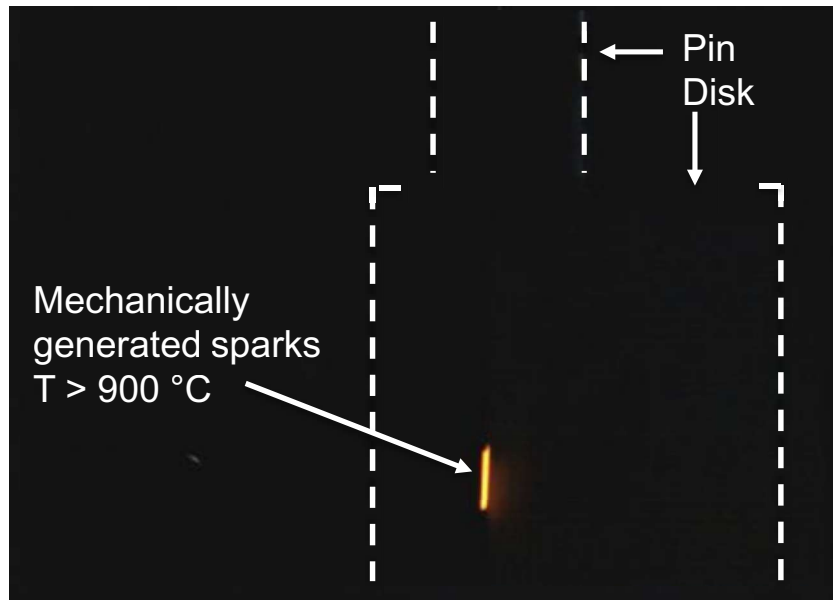
# Ignition source

The ignition source depends on the material:

**Mechanically generated sparks**

and resulting explosion:

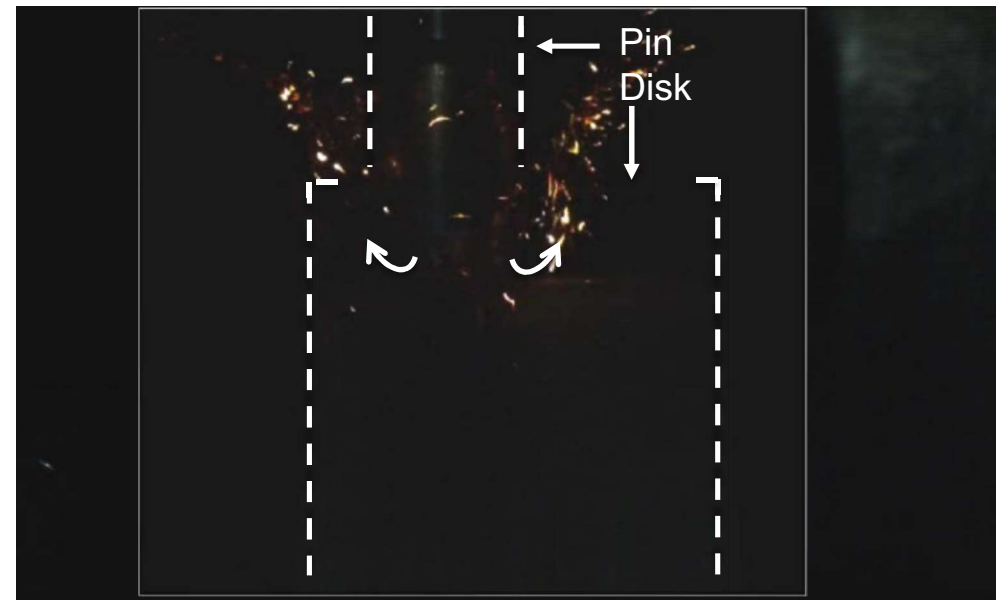
Concrete (disk) vs. Mild Steel 1.0038 (pin)



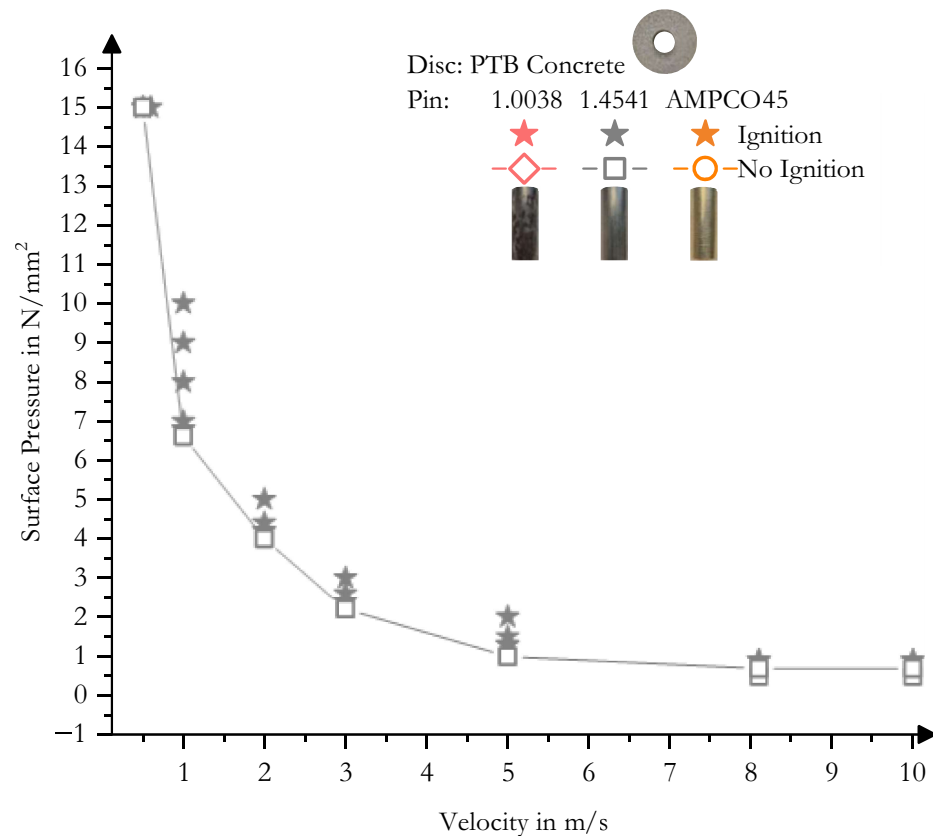
Explosion starts at the **hot surface**:

Concrete (disk) vs. Stainless Steel 1.4541 (pin) und

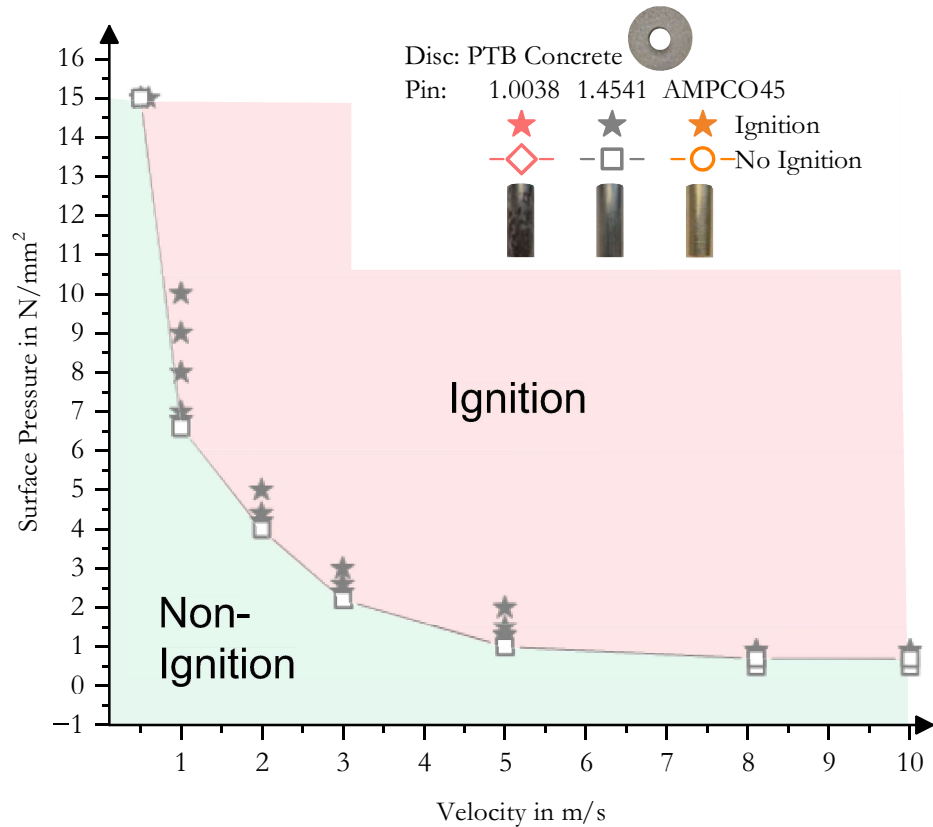
Concrete (disk) vs. Aluminium Bronze(pin)



# Ignition limit curves

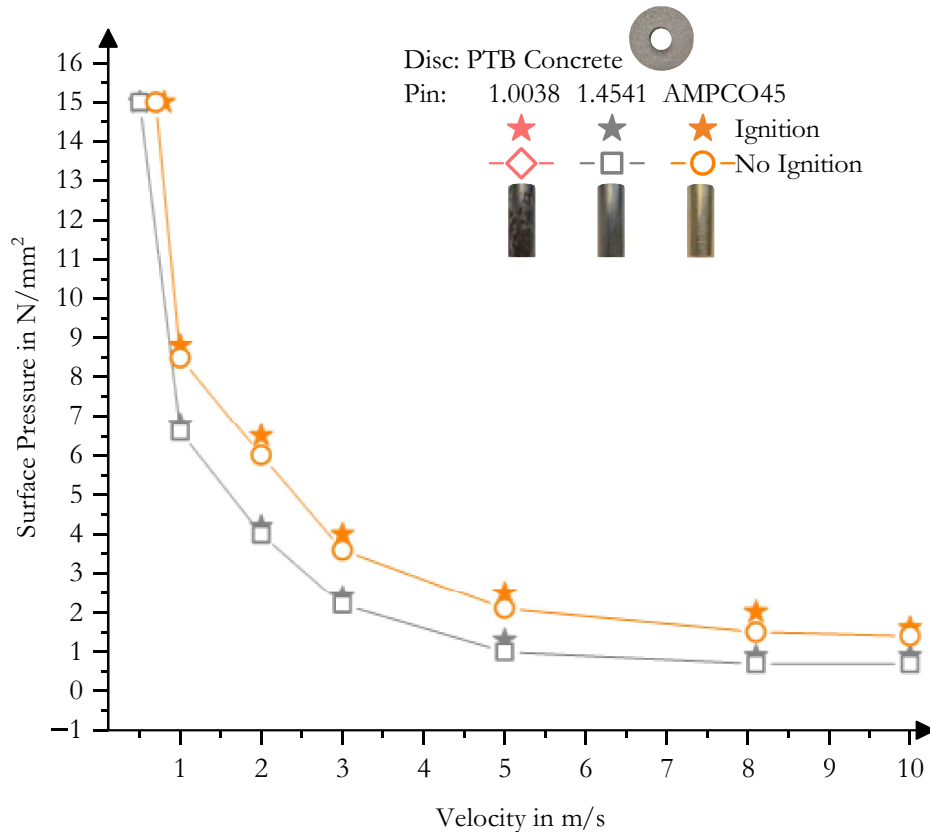


# Ignition limit curves



Based on the Ignition limit curve, we can separate between an "Ignition" and "Non-Ignition" area

# Ignition limit curves



Stainless Steel 1.4541 compared with  
Aluminium Bronze AMPCO 45:

Heat conductivity :

Stainless Steel 1.4541

15 W/m·K

Aluminium Bronze AMPCO 45

45 W/m·K

→ The lower heat conductivity of stainless steel causes ignition due to the hot surface at lower combinations of surface pressure and velocity.

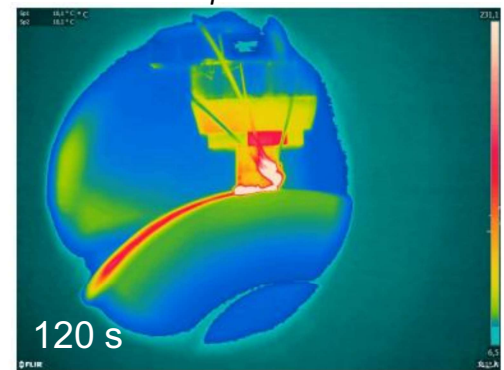
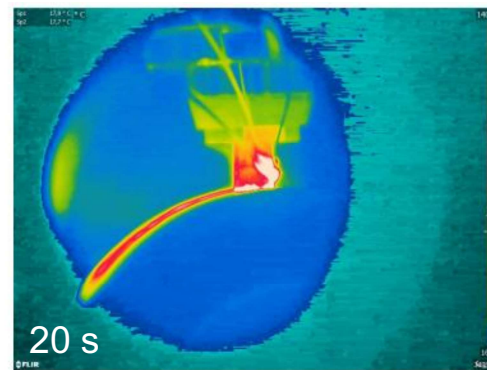
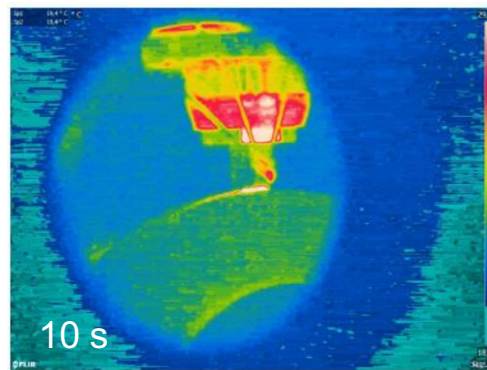
# Ignition source

The temperature distribution depends on the material:

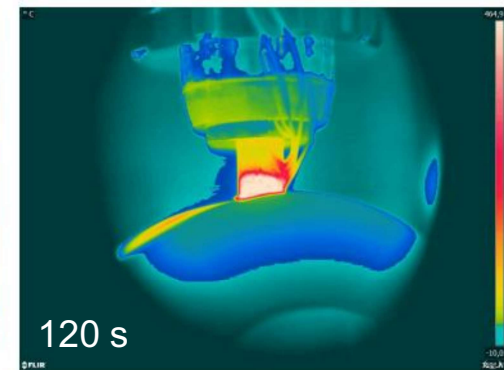
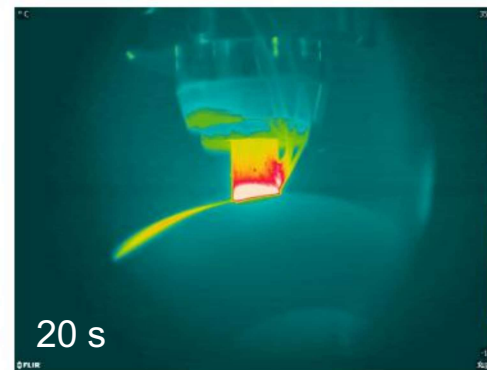
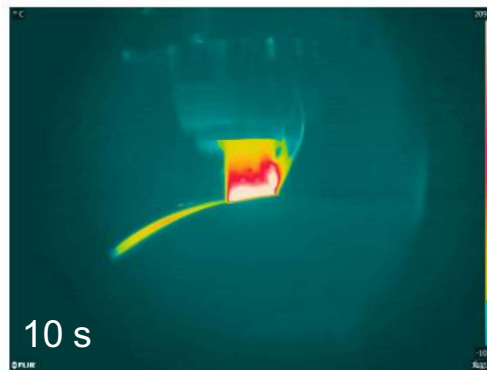
A lower heat conductivity leads to a hotspot at the contact point  $\rightarrow \lambda \downarrow = T_{\text{contact point}} \uparrow$

$v = 5 \text{ m/s}, p = 2 \text{ N/mm}^2$

**Aluminium  
Bronze  
AMPCO45**  
 $\lambda = 45 \text{ W/m}\cdot\text{K}$

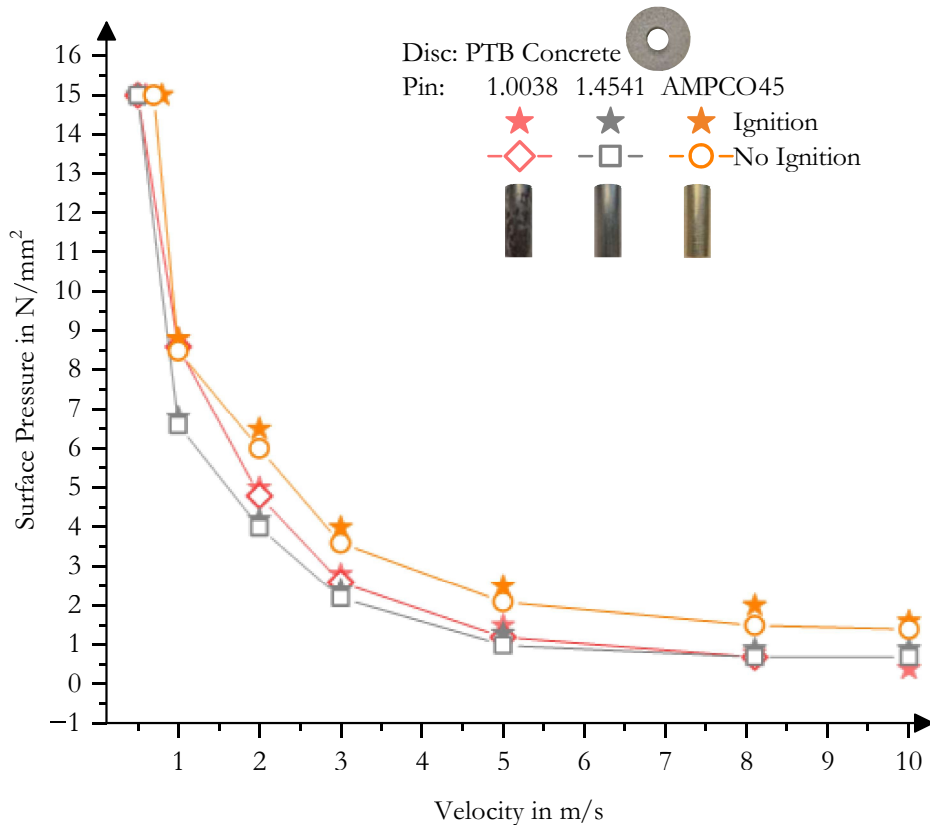


**Stainless  
Steel  
1.4541**  
 $\lambda = 15 \text{ W/m}\cdot\text{K}$





# Ignition limit curves



Stainless Steel 1.4541 and  
Aluminium Bronze AMPCO 45  
in comparison with Mild Steel 1.0038:

Heat conductivity :

Stainless Steel 1.4541

15 W/m·K

Aluminium Bronze AMPCO 45

45 W/m·K

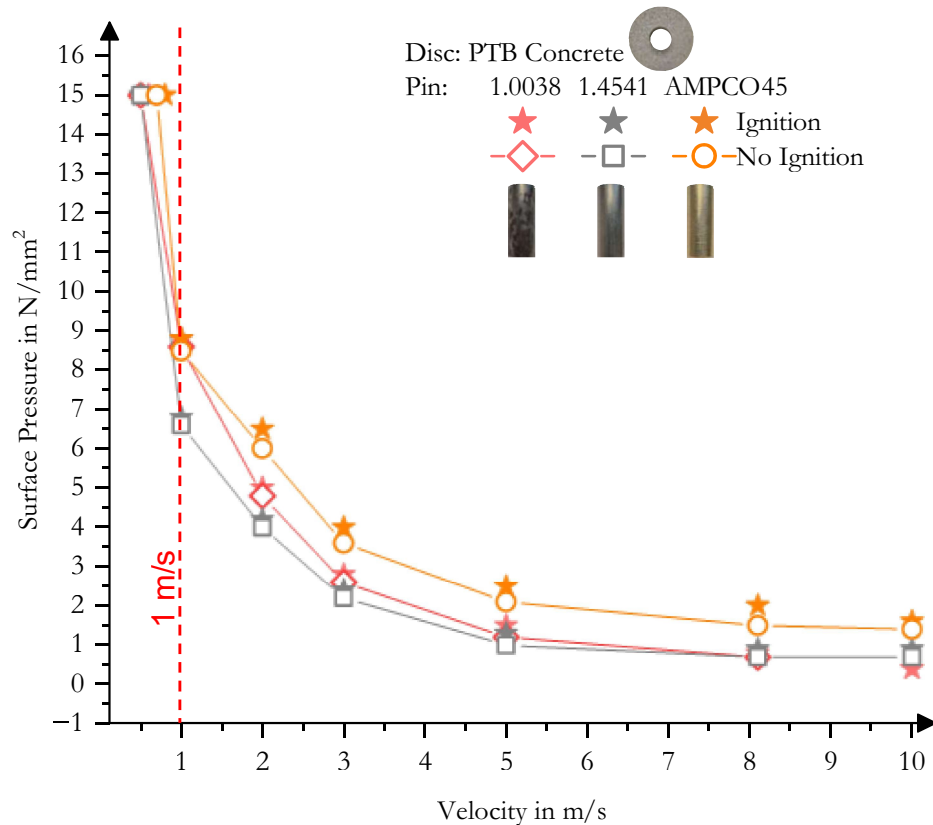
Mild Steel 1.0038

60 W/ m·K

→ Mild Steel:

Due to its carbon content, it does not  
ignite from a hot surface, but rather from  
mechanically generated sparks

# Ignition limit curves



## ISO 80079-36:2016:

„A relative contact speed of **1 m/s** is often used as the limit value below which friction ignition sources are not capable to ignite an explosive atmosphere. ... There are a few exceptions, for example... explosive gas atmospheres such as hydrogen ..., where there is a high contact load.,”



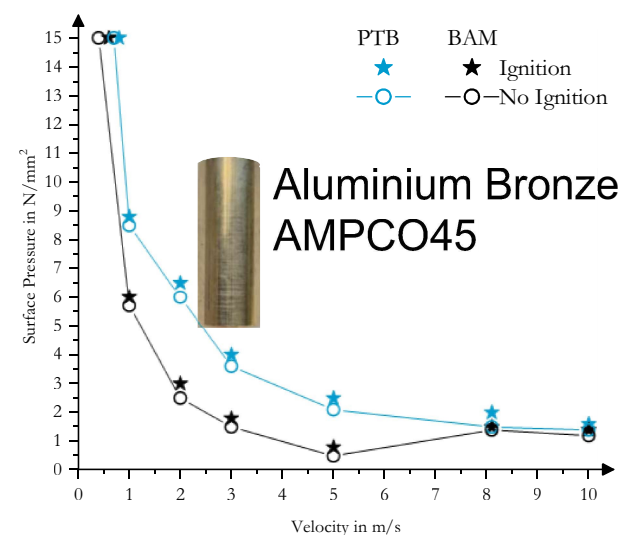
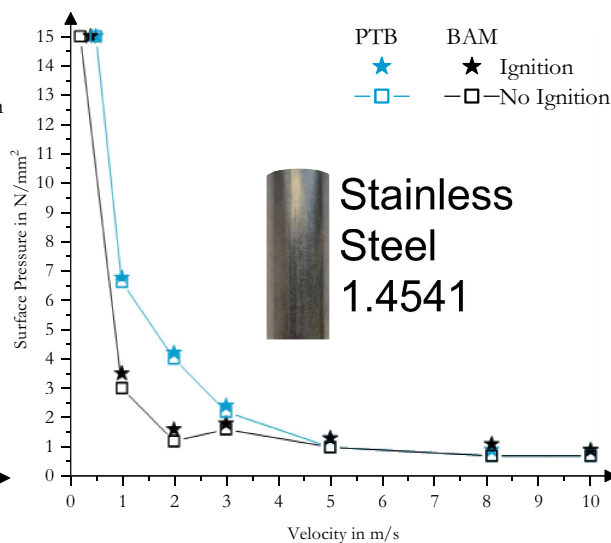
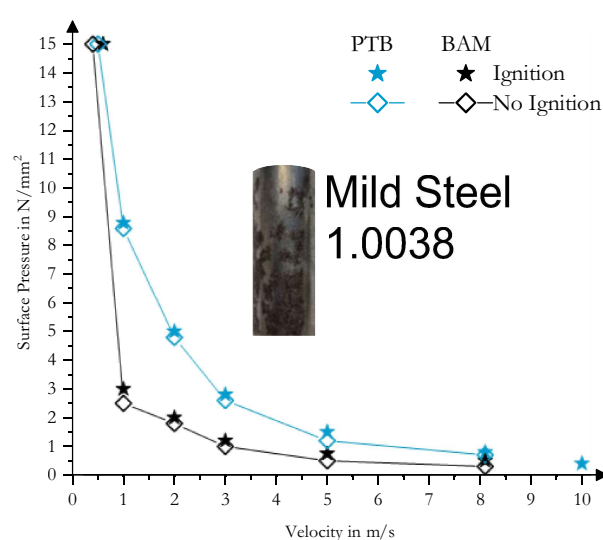
# Ignition limit curves



PTB-Concrete



BAM- Concrete  
without Corundum



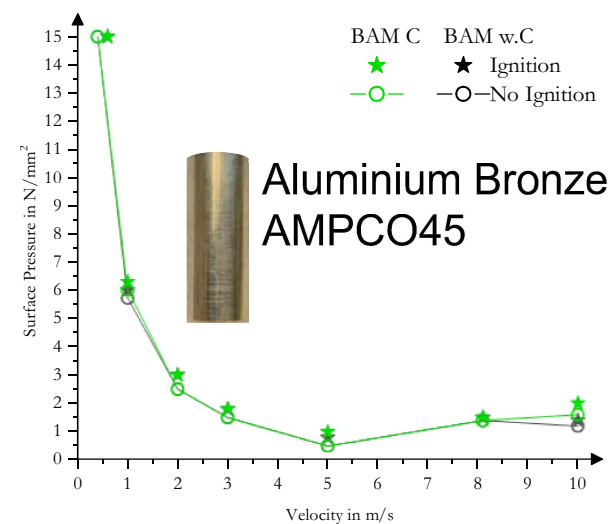
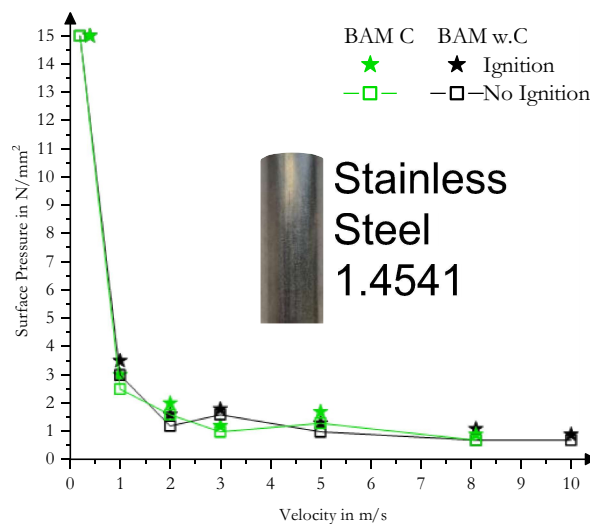
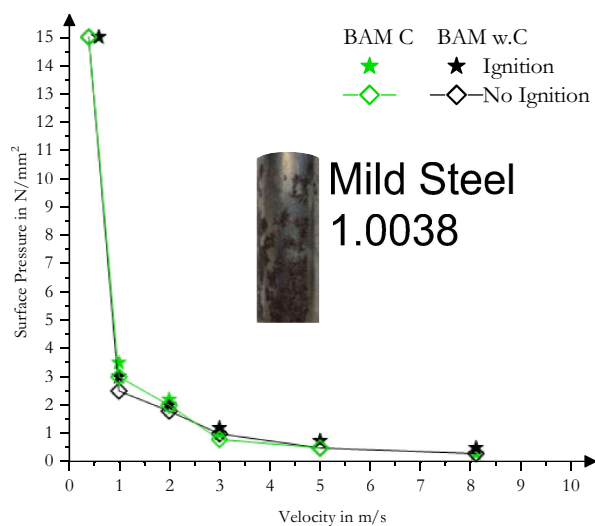
# Ignition limit curves



BAM-Concrete  
with 5% Corundum  
(BAM C)



BAM-Concrete  
without Corundum  
(BAM w.C)

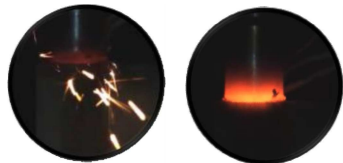


# Conclusions



Applying concrete disks into the test setup:

- Pore water → Drying of the concrete disks (24 h at 120 °C)

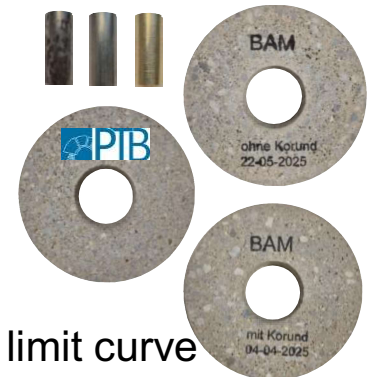


The ignition source depends on the material:

- Mild Steel 1.0038 → Mechanically generated sparks
- Stainless Steel 1.4541 & Aluminium Bronze AMPCO45 → Hot surface

Ignition limit curves (surface pressure over velocity):

- Determined for material combinations of Metal (pin) and Concrete (disk)
- Stainless steel has low heat conductivity (15 W/m·K) and is more inclined to form hot surfaces than Aluminium Bronze (45 W/m·K)
- Ignition is possible at velocities below 1 m/s with high surface pressures
- BAM-Concrete is more ignitable than PTB-Concrete! Why?
- 5% Corundum in the concrete has no effect on ignition source and ignition limit curve







Physikalisch-Technische Bundesanstalt  
Braunschweig and Berlin

Bundesallee 100  
38116 Braunschweig

Dr. Florian Baumann

Phone: 0531 592-3731

E-Mail: [florian.baumann@ptb.de](mailto:florian.baumann@ptb.de)  
[www.ptb.de](http://www.ptb.de)

Dr. Carola Schierding

Phone: 0531 592-3730

E-Mail: [carola.schierding@ptb.de](mailto:carola.schierding@ptb.de)  
[www.ptb.de](http://www.ptb.de)

State: 03/26